



# **Dissemination of the heating technology research results for emission minimization and process optimization towards today's fossil-free heating agenda**

RFCS-2021

Grant agreement no. 101057930

## **Report with categorized applications and technologies for low CO<sub>2</sub> heating**

Deliverable 2.3

### Authors

Elsa Busson, Nico Schmitz, Thomas Echterhof, Joel Falk, Andreas Johnsson, Gustav Häggström, Oliver Hatzfeld, Filippo Avellino, Davide Ressegotti, Hugo Uijderbroeks

Dissemination level: Public

Version 2.0

Published 2023-11-29

## Content

1	Introduction .....	4
2	Methods .....	5
3	List of high TRL technologies for low CO <sub>2</sub> heating.....	7
3.1	Topic 1: Heating and burner technology .....	9
3.1.1	Self-recuperative burners .....	9
3.1.2	Regenerator burner, regenerative air preheating through off-gas heat recovery .....	10
3.1.3	Oxy-fuel combustion .....	10
3.1.4	Oxygen lancing .....	11
3.1.5	Fossil free CH <sub>4</sub> .....	11
3.1.6	Fuel preheating of blast furnace gas with or without oxy-fuel combustion/OEC.....	11
3.1.7	Indirect resistive heating .....	12
3.1.8	Inductive heating.....	12
3.2	Topic 2: Modelling of entire furnace, Level-2 control .....	12
3.2.1	Diagnostics, Warning and Suggestion system (DWS) .....	12
3.2.2	Dynamic Furnace Model .....	12
3.2.3	Furnace Model coupled to microstructural model .....	12
3.3	Topic 3: Sensors and controls (Level-1), standards, regulations.....	13
3.3.1	Air ratio controller.....	13
3.3.2	Acid Dew Point sensor (ADP) .....	13
3.4	Topic 4: Materials in the furnace and product quality .....	13
3.4.1	Coating application .....	13
3.4.2	High emissivity coatings for furnace refractory.....	13
3.5	Topic 5: Heat transfer, heat recovery, productivity, economy .....	14
3.5.1	Waste heat boiler .....	14
3.5.2	Feedstock preheating .....	14
3.5.3	Warm or hot charging in rolling mills not coupled to continuous casting	14
3.5.4	Direct charging in coupled continuous casting and rolling .....	14
4	List of emerging technologies for low CO <sub>2</sub> heating .....	15
4.1	Topic 1: Heating and burner technology .....	16
4.1.1	Multi-fuel burner for reheating furnaces .....	16
4.1.2	Biofuels as a fuel for reheating furnaces.....	16
4.1.3	Hydrogen as a fuel for reheating processes .....	17
4.1.4	Ammonia as a fuel for reheating processes.....	17

---

4.1.5 Plasma heating .....	17
4.1.6 Direct resistive heating.....	18
4.2 Topic 2: Modelling of entire furnaces, Level-2 control .....	18
4.2.1 Online Furnace Model coupled to microstructural model .....	18
4.3 Topic 3: Sensors and controls (Level-1), standards, regulations.....	18
4.4 Topic 4: Materials in the furnace and product quality .....	18
4.5 Topic 5: Heat transfer, heat recovery, productivity, economy .....	18
4.5.1 Organic Rankine cycle .....	18
4.5.2 Thermoelectric generator .....	18
4.5.3 CCS/CCU .....	19
5 References .....	20

## 1 Introduction

The DissHEAT project evaluates and promotes research carried out over the last 20 years in the field of reheating technology in the steel industry. To this end, past projects have been critically reviewed and categorised into different topics.

The processing of ferrous and non-ferrous metals in reheating furnaces is always aimed at achieving the best possible product quality while minimising costs, air pollution and, in recent years, CO<sub>2</sub> emissions. In this document, several state of the art and emerging, low TRL reheating technologies relevant to low CO<sub>2</sub> heating have been identified.

The identified technologies are divided into technologies with high TRLs above 7 and emerging technologies with TRLs below 7. The review of the technologies is mainly based on the CO<sub>2</sub> reduction potential, but also considers the impact on auxiliary equipment and economic implications. Advantages and disadvantages are listed for the technologies.

The identified technologies are classified into five different topics:

1. Heating and burner technology
2. Modelling of entire furnaces, Level-2 control
3. Sensors and controls (Level-1), standards, regulations
4. Materials in the furnace and product quality
5. Heat transfer, heat recovery, productivity, economy

## 2 Methods

Due to the limited availability of quantified CO<sub>2</sub> emission reduction figures, the technologies are further categorised according to their area of action for CO<sub>2</sub> reduction to provide an approximation of their potential. To illustrate these potentials, the energy flows of a pusher-type furnace heated with natural gas, coke oven gas and air are presented as an example in a Sankey-diagram in Figure 1. Considering a carbon intensity of 200.88 gCO<sub>2</sub>/kWh for natural gas and 147.6 gCO<sub>2</sub>/kWh for coke oven gas [1], the total CO<sub>2</sub> footprint of this furnace is approximately 59.34 kgCO<sub>2</sub>/t<sub>steel</sub>. Several measures can be adopted to reduce the CO<sub>2</sub> footprint of the furnace, but these measures have different degrees of impact. In the following, the CO<sub>2</sub> emission reduction potential has been calculated for different areas of the furnace to illustrate the level of impact the different technologies can have. To keep the calculation simple, it has been assumed that the measures have no effect on the other energy flows in the furnace. However, in a real application, most changes in the process can affect the rest of the furnace energy balances. The goal of the calculation is to give an order of magnitude for the different areas of action for the CO<sub>2</sub> reduction.

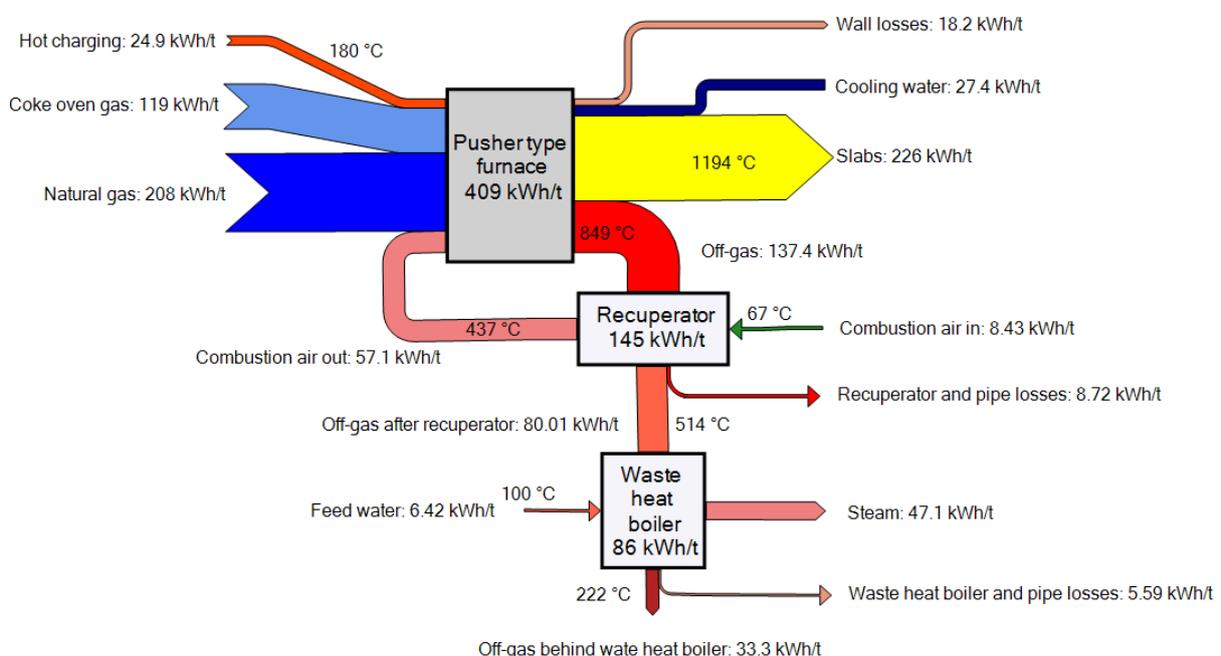


Figure 1: Sankey-diagram of a pusher-type furnace, 2005 [2]

A first area for CO<sub>2</sub> emission reduction measure is furnace losses. Reducing the losses leads to a reduction in the fuel consumption of the furnace. For example, reducing the furnace losses by half could reduce the CO<sub>2</sub> emission of the furnace by approximately 1.65 kgCO<sub>2</sub>/t<sub>steel</sub> (2.8%).

Another area of action would be to reduce the fuel consumption by increasing the temperature of the preheated air. This could be achieved, for example, by improving the efficiency of the recuperator. For combustion air temperatures of up to 650 °C [3] there is a potential reduction in CO<sub>2</sub> emissions of up to 5 kgCO<sub>2</sub>/t<sub>steel</sub> (8%) in this case.

Another possibility to reduce the fuel consumption of the furnace is to increase the temperature of the charged slabs to, e. g., 400 °C. This increase in slab temperature would result in a reduction in CO<sub>2</sub> emissions of approximately 5.4 kgCO<sub>2</sub>/t<sub>steel</sub> (9%). For the sake of simplicity, the calculation was made assuming that the total energy demand

and capacity of the furnace didn't change. However, changing the temperature of the slab would have a non-negligible impact on both.

Finally, the substitution of carbon intensive fuels with carbon free fuels or electricity would have a much more significant impact on reducing CO<sub>2</sub> emissions than the previous technologies. It could potentially reduce the CO<sub>2</sub> emission of the furnace to almost zero, assuming the use of green energy.

### 3 List of high TRL technologies for low CO<sub>2</sub> heating

This section describes high TRL (> 7) technologies that help reduce the CO<sub>2</sub> emissions from reheating furnaces.

Table 1: Overview of high TRL technologies for low CO<sub>2</sub> heating

Identified technology	Related topic	TRL today	Area of action for CO <sub>2</sub> reduction	CO <sub>2</sub> emission reduction (scope 1)	CO <sub>2</sub> emission reduction (scope 2)
<b>Self-recuperative burners [4]</b>	1	9	Fuel savings by reducing off-gas heat losses through heat recovery.	Equivalent to fuel savings. Up to 30% fuel savings compared to cold air combustion.	No significant impact.
<b>Regenerator burners, regenerative air preheating through off-gas heat recovery [5–8]</b>	1	9	Fuel savings by process internal heat recovery from off-gases.	From 12% to 40% compared to recuperative systems with an average of 300 °C recuperative preheated air.	No significant impact.
<b>Oxy-fuel combustion [9,10]</b>	1	9	Fuel savings by decreasing off-gas heat losses.	From 20% to 60%.	No significant impact.
<b>Oxygen lancing [11–13]</b>	1	9	Fuel savings by decreasing off-gas heat losses.	From 15% to 30%.	No significant impact.
<b>Fossil free CH<sub>4</sub></b>	1	9	Substitution from fossil fuels with a low CO <sub>2</sub> energy source.	No direct emissions if the carbon is biogenic.	Electricity based CH <sub>4</sub> would be similar to H <sub>2</sub> based on electrolysis. No numbers available for biomass-based methane.
<b>Fuel preheating of blast furnace gas with or without oxy-fuel combustion/OEC [14]</b>	1	7-8	<ul style="list-style-type: none"> <li>Substitution of natural gas by process gases in heating processes.</li> <li>Increased efficiency by heat recovery from exhaust gases.</li> </ul>	50-60 kg <sub>CO2</sub> /t <sub>steel</sub> assuming the BFG has no CO <sub>2</sub> footprint.	No significant impact.

Identified technology	Related topic	TRL today	Area of action for CO <sub>2</sub> reduction	CO <sub>2</sub> emission reduction (scope 1)	CO <sub>2</sub> emission reduction (scope 2)
<b>Indirect resistive heating [15]</b>	1	4-9	Substituting fossil fuels with a (potentially) low CO <sub>2</sub> energy source.	No direct emissions.	No impact.
<b>Inductive heating [16,17]</b>	1	4-9	Substituting fossil fuels with a (potentially) low CO <sub>2</sub> energy source.	No direct emissions.	Higher than electric resistive heating due to lower efficiency.
<b>Diagnostics, Warning and Suggestion system (DWS) [18]</b>	2	7	CO <sub>2</sub> reduction by fuel saving, obtained by decreasing heat demand to achieve target temperature.	Up to 3% reduction in CO <sub>2</sub> emissions.	No impact.
<b>Dynamic Furnace Model [19]</b>	2	7	CO <sub>2</sub> reduction by fuel saving.	From 3% to 6% reduction in CO <sub>2</sub> emissions for high productivity (> 350 t per day) and from 7% to 13% for low productivity (< 350 t per day).	No impact.
<b>Furnace Model coupled to microstructural model [20]</b>	2	7	CO <sub>2</sub> reduction by fuel saving.	Decrease CO <sub>2</sub> emissions up to 7%.	No impact.
<b>Air ratio controllers [21]</b>	3	9	Fuel savings by reducing off-gas losses through minimum excess air.	From 2% to 6% depending on the furnace.	No impact.
<b>ADP Sensor [22]</b>	3	8-9	Fuel savings by reducing off-gas losses through heat recovery.	720 kt <sub>CO2</sub> /y for European steel industry.	No impact.
<b>Coating application</b>	4	9	Material saving by reducing scale formation.	Not available.	No impact.

Identified technology	Related topic	TRL today	Area of action for CO <sub>2</sub> reduction	CO <sub>2</sub> emission reduction (scope 1)	CO <sub>2</sub> emission reduction (scope 2)
<b>High emissivity coatings for furnace refractory [23]</b>	4	9	CO <sub>2</sub> reduction by fuel saving.	Up to 5%.	No impact.
<b>Waste heat boiler [4]</b>	5	9	Substitution from the fuel that would otherwise be used to produce hot water/steam/electricity.	No direct emissions.	Depends on the fuel that is substituted by the hot water/steam/electricity produced.
<b>Feedstock preheating [4]</b>	5	9	Fuel savings by reducing off-gas losses through heat recovery	Depends on the extent the feedstock can be preheated. Fuel savings of 20% have been reported for preheating the feedstock from ambient temperature to 400 °C.	No impact.
<b>Warm or hot charging in rolling mills not coupled to continuous casting [4]</b>	5	8-9	Increased efficiency by avoiding heat loss: The heating process starts with a product at high temperature instead of ambient temperature.	19% when charging the product at 400 °C.	No impact.
<b>Direct charging in coupled continuous casting and rolling mills [4]</b>	5	9	Increased efficiency by avoiding heat loss: The heating process starts with a product at high instead of ambient temperature.	39% when charging the product at 750 °C.	No impact.

### 3.1 Topic 1: Heating and burner technology

#### 3.1.1 Self-recuperative burners [4]

This technology consists of preheating the combustion air by sensible heat recovery from the off-gas. This technology is only applicable for air combustion and cannot be used to reach high air preheating temperatures. Self-recuperative burners are typically

not used in pusher-type and walking beam furnaces due to the required burner sizes and powers. However, they are commonly used for the reheating process of thin-slabs in tunnel furnaces after thin-slab casting.

### **3.1.2 Regenerator burner, regenerative air preheating through off-gas heat recovery [5–8]**

This technology consists of burners with integrated ceramic accumulators that transfer off-gas heat to the combustion air. Air preheating of above 1,000 °C is achieved and up to 80% of the off-gas heat is recovered for process heating.

The burner systems are state of the art and are available from most burner suppliers.

Different types of burners are available: conventional flame burners with ultra-low NO<sub>x</sub>-systems and flameless burners. In addition, the shape of the flame can vary from flat to long with high momentum.

Regenerators are mainly operated in an on/off mode with ceramic ball-fill/different shaped parts for fills or ceramic honeycomb accumulators. Regenerators can also be used in continuous systems with rotating honeycomb accumulators.

The benefits of regenerators are as follows:

- They increase the efficiency of the heating processes by recovering heat from off-gas and providing high combustion air pre-heating, thereby reducing operating costs and CO<sub>2</sub> emissions.
- They increase the productivity and reduce the specific energy consumption (e.g. kWh/t) by reducing the heating time in the furnace by achieving higher furnace temperature in the heating zone.
- Flameless combustion is possible for low NO<sub>x</sub> combustion with NO<sub>x</sub> emissions below 150 ppm (for 3 vol% O<sub>2</sub> in the off-gas).
- They help increased heating uniformity. When operating in a flameless combustion mode and if there is sufficient space above or below the product in the furnace, increased uniform heating of the product can be achieved compared to combustion with flames.

However, regenerators also have disadvantages. Investments costs are higher than for recuperative heating systems. Additional maintenance is required to clean the ceramic accumulators, depending on the type of regenerator.

In comparison with recuperative burners with an average of 300 °C recuperative preheated air, reduction in CO<sub>2</sub> emissions of between 12% and 40% have been reported.

### **3.1.3 Oxy-fuel combustion [9,10]**

Oxy-fuel combustion consists in burning a fuel using pure oxygen instead of air as the oxidiser. The absence of nitrogen in the oxidiser significantly reduces the off-gas volume as well as the energy losses through the off-gas. This increases the thermal efficiency of the system and the radiative heat transfer due to the higher concentration of highly radiative CO<sub>2</sub> and H<sub>2</sub>O particles in the furnace atmosphere.

When installing oxy-fuel combustion systems, consideration must be given to the tightness of the furnace and proper pressure regulation to prevent air leakage resulting in significant NO<sub>x</sub> emissions. If the furnace is operated carefully, low NO<sub>x</sub> emissions can be achieved. If ambient air enters the furnace, high NO<sub>x</sub> emission will result due to the high combustion temperature of oxy-fuel. Flameless oxy-fuel application has

also been investigated to reduce NO<sub>x</sub> emissions. In addition, the use of oxy-fuel requires a complete retrofit of the burner technology. However, retrofitting has been done many times and is a well-known technology.

The disadvantages of using oxyfuel include the higher cost of running pure oxygen, which has to be considered. The economics need to be assessed on a case-by-case basis.

Fuel consumption reductions of around 20 to 26% and CO<sub>2</sub> emission reductions of 15% have been reported. A further 20 to 30% improvement in throughput has been reported for semi-flameless oxyfuel applications.

#### **3.1.4 Oxygen lancing [11–13]**

Oxygen lancing consists in installing oxygen lances on the furnace walls near the burners. Oxygen is injected into the furnace at high velocity through the lances. Approximately 75% of the combustion air is replaced by the oxygen. Oxygen lancing reduces the off-gas volume by 50%, thereby reducing off-gas losses. Reduction in fuel consumption of 11% and 15% have been reported, which also reduces CO<sub>2</sub> emission from the furnace. In addition, the oxygen lancing was reported to have minimum impact on NO<sub>x</sub> emission, scale formation on the slab furnace and it improves production capacity by up to 20%. The technology requires low maintenance and the investment costs are low if existing air equipment can be re-used.

#### **3.1.5 Fossil free CH<sub>4</sub>**

This technology consists of replacing fossil fuel with CH<sub>4</sub> produced from electricity or biomass. This technology doesn't reduce local CO<sub>2</sub> emissions at the furnace, but in the overall balance of the system, the net CO<sub>2</sub> emission are zero if the biogenic carbon is rated net-zero.

The advantages of fossil free methane are that it is easy to add to the fuel and can be implemented without major modifications to existing reheating furnaces. In addition, biomass-derived methane is currently potentially cost-competitive with fossil fuels.

However, this technology can be potentially expensive depending on the price of biomass and electricity. Due to losses associated with the production of the fuel, the cost would be higher than using electricity directly for heating.

#### **3.1.6 Fuel preheating of blast furnace gas with or without oxy-fuel combustion/OEC [14]**

This technology involves recuperative fuel preheating of low calorific process gases in integrated steel mills. It is interesting to note, that regenerative fuel preheating is not possible for safety reasons, as regenerators always have leakage.

The reduction in CO<sub>2</sub> emissions is achieved by substituting natural gas for process gases and by increasing the efficiency of the systems through heat recovery of the off-gas. Increasing efficiency also reduces operating costs. However, investments costs are high due to the need for additional plant components.

As an application, a 150 t/h reheating furnace in steel mill currently is working with 80% Blast Furnace Gas (BFG). The reduction in CO<sub>2</sub> emission is 50-60 kgCO<sub>2</sub>/t<sub>steel</sub>, assuming that the BFG application in the reheating process has no CO<sub>2</sub> footprint.

### **3.1.7 Indirect resistive heating [15]**

This technology consists of reheating steel using electric radiant heaters. A few industrial scale implementations already exist, but they are rare and typically operate at temperatures below 1,000 °C. One of the advantages of this technology is the low specific energy consumption per ton of feedstock (high efficiency). In addition, the furnace control system is relatively simple and achieves high precision (low  $\Delta T$ ). However, the cost of electricity is typically higher compared to fossil fuels, and the power density of electric radiant heaters at higher temperature is low compared to combustion-based systems, thus requiring more space.

### **3.1.8 Inductive heating [16,17]**

This technology consists of reheating steel using inductive heaters. There are a few industrial-scale implementations, but they are rare and typically operate at temperatures below 700 °C.

The advantage of this technology is that very high heating rates can be achieved (high energy density). However, this technology is inflexible in terms of feedstock geometry and efficiency is relatively low compared to other electrical heating solutions. Finally, the process is difficult to optimise for a wide temperature range, as the conductivity and ferromagnetic properties of steel vary with temperature.

## **3.2 Topic 2: Modelling of entire furnace, Level-2 control**

### **3.2.1 Diagnostics, Warning and Suggestion system (DWS) [18]**

This system consists of a database for data collection and both physical and statistical models to suggest improvement in operating practices or to detect operating errors (e.g. burner imbalance). The reduction in CO<sub>2</sub> emissions is achieved by reducing the amount of heat required to achieve the target temperature, thus reducing fuel necessity. CO<sub>2</sub> emission reduction up to 3% have been reported in SSAB's hot strip mill slab furnace. This technology can be implemented without major modifications to existing reheating furnaces. However, it requires an extensive data collection system and time to tune a reliable warning system and model.

### **3.2.2 Dynamic Furnace Model [19]**

This technology consists of a dynamic model to monitor and control the temperature and oxygen content of the reheating furnaces, even during stoppages and interruptions. As for the DWS, the technology can be implemented without major modifications to existing reheating furnaces, but requires an extensive data collection system and time to tune a reliable system and model. In addition, more temperature and oxygen measurement systems will need to be implemented for the model. The reduction in CO<sub>2</sub> emissions will be achieved by reducing fuel consumption. A reduction of 3% to 6% has been reported for high productivity furnaces (more than 350 t per day) and between 7% and 13% for low productivity furnaces (less than 350 t per day).

### **3.2.3 Furnace Model coupled to microstructural model [20]**

This model consists of an off-line model to simulate the thermal behaviour and microstructure of the product with the aim of developing optimised operating practices. As for the preceding technologies, the system can be easily implemented in existing furnaces, but requires extensive data collection and time to achieve a reliable model. The system can achieve CO<sub>2</sub> emission reductions of up to 7%. A system has been

implemented and tested at ACRONI (implementation of new reheating strategies) and Sidenor (improvement of heating time to reach drop-out temperature).

### **3.3 Topic 3: Sensors and controls (Level-1), standards, regulations**

#### **3.3.1 Air ratio controller [21]**

Air ratio controllers are a well-known system for optimising the oxygen content in the furnace, thereby reducing off-gas heat losses. They can be pneumatic or electrical, or the controller can be implemented in an industrial controller or PLC. Depending on the furnace, CO<sub>2</sub> emissions can be reduced by between 2% and 6%, as fuel consumption can be reduced by minimising off-gas losses through minimum excess air content.

#### **3.3.2 Acid Dew Point sensor (ADP) [22]**

Acid Dew Point (ADP) sensors are used to monitor the concentration of sulfuric acid in stack gases. ADP sensors work by cooling a sensor, causing a sulfuric acid film to form on its surface when it is cooled below the ADP. The conductivity between the sensor's ring electrode and the thermocouple indicates the thickness of the film. When the sensor is at the ADP temperature, the rates of evaporation and deposition are equal, so the thickness of the film and, hence, its conductivity are constant. This product is available from several manufacturers (Ametek, Walsn, Sidph). This technology has the potential to reduce the European steel industry's CO<sub>2</sub> emissions by 720 ktCO<sub>2</sub>/year.

The advantages of this technology are as follow:

- Optimised off-gas temperature and improved waste heat recovery efficiency.
- Reduced cold-end corrosion in heat exchangers, ducts and stacks resulting in fewer maintenance problems.
- Reduced sulphate aerosol emissions.

It is important to note that detection of ADT can be slow at very low sulphuric acid concentrations.

### **3.4 Topic 4: Materials in the furnace and product quality**

#### **3.4.1 Coating application**

In most long product mills, a protective glass coating is applied to the surface of the product before it enters the reheating furnace. This has a significant impact on the quality of the steel and therefore the number of downgraded materials.

The use of coatings to reduce oxide formation in reheating furnaces has been widely investigated. The current state of the art is that an oxide layer of approximately 300 µm is formed after casting and during reheating. This results in a material loss of 1 to 2% or 1.5 €/t. Limiting oxidation reduces the amount of steel required and therefore the CO<sub>2</sub> emissions in primary processing.

Laboratory studies have shown that the use of coatings can reduce scale formation by 40% and even 100%. However, there is an important limitation related to the grade. Coatings must be adapted to each steel family. If a particular coating reduces scale formation on low carbon grades, it may increase it on high strength grades.

#### **3.4.2 High emissivity coatings for furnace refractory [23]**

High emissivity coatings are a well-established technology in small furnaces. Energy savings of up to 5% can be achieved compared to uncoated refractory. It is not used

in large reheating furnaces, such as hot strip mills, due to the complexity of application and the wear resistance of the coating.

### **3.5 Topic 5: Heat transfer, heat recovery, productivity, economy**

#### **3.5.1 Waste heat boiler [4]**

This technology consists of sensible heat recovery from the off-gas to produce hot water/steam and/or electricity. This technology doesn't reduce the specific energy consumption per ton of steel and requires a demand for hot water/steam.

#### **3.5.2 Feedstock preheating [4]**

This technology consists of preheating the feedstock through convective heat transfer (direct contact) from the off-gases. This helps decrease the fuel consumption by improving the utilization of sensible heat in the off-gas (at low temperature). However, feedstock preheating is generally not possible for batch processes and the utility of feedstock preheating decreases as the temperature of the incoming feedstock increases.

#### **3.5.3 Warm or hot charging in rolling mills not coupled to continuous casting [4]**

This technology consists of storing the product from the continuous casting after the cutting process in insulated boxes or under insulated hoods for later charging in the reheating furnace of the rolling mill at temperatures between 300 and 600 °C.

The necessary insulated hoods and boxes are available or can be built by suppliers.

By shortening the time between casting and reheating and/or insulating the feedstock during transfer, the feedstock enters the reheating furnace at a higher temperature, lowering the energy demand for heating. This technology therefore helps reduce the CO<sub>2</sub> emissions and operating costs of the plant.

However, this technology requires space close to the reheating furnace, well-planned production cycles and higher costs for low-tech components. Furthermore, it limits the possibility of using feedstock preheating and increases stack temperature, which can lead to a decrease in the efficiency of furnaces which utilise recuperative systems and feedstock preheating. It can also result in significant variation in the temperature of feedstock going into the furnace which can present a problem for the control system of the reheating furnace in terms of temperature variation.

#### **3.5.4 Direct charging in coupled continuous casting and rolling [4]**

This technology consists of feeding the product from the continuous casting after the cutting process directly into the reheating furnace of the rolling mill at temperatures between 600 and 850 °C.

This technology helps to improve production efficiency, reduce CO<sub>2</sub> emissions and lower operating costs. However, this technology is only suitable for production processes with little or no change in product or product quality. In addition, a complete production process study is required.

Continuous steel casting and rolling mills are available from suppliers.

The TRL of this technology varies depending on the feedstock geometry. For long products with small dimensions the TRL is high, but for other types of feedstock geometries it is low. Inductive heating units are available from 20 to 50 MW (i.e. ABP induction).

## 4 List of emerging technologies for low CO<sub>2</sub> heating

This section describes low TRL (< 7) technologies that help could potentially reduce the CO<sub>2</sub> emissions from reheating furnaces.

Table 2: Overview of low TRL technologies for low CO<sub>2</sub> heating

Identified technology	Related topic	TRL today	Area of action for CO <sub>2</sub> reduction	CO <sub>2</sub> emission reduction (scope 1)	CO <sub>2</sub> emission reduction (scope 2)
<b>Multi-fuel burner for reheating furnaces [24,25]</b>	1	5-6	Substitution from fossil fuels with a low CO <sub>2</sub> energy source.	No direct emissions when using hydrogen or ammonia as gas.	Depending if the energy is produced by renewable sources.
<b>Biofuels as a fuel for reheating furnaces [26]</b>	1	5-9, depending on the gas	Substitution from fossil fuels with a low CO <sub>2</sub> energy source.	100% if the carbon is biogenic.	No emissions if the energy is produced by renewable sources.
<b>Hydrogen as a fuel for reheating process [27–29]</b>	1	7	Substitution from fossil fuels with a low CO <sub>2</sub> energy source.	No direct emissions.	100 % if energy is produced by renewable sources.
<b>Ammonia as a fuel for reheating process [30,31]</b>	1	4-5	Substitution from fossil fuels with a (potentially) low CO <sub>2</sub> energy source.	No direct emissions.	Electricity based NH <sub>3</sub> would be similar to H <sub>2</sub> based on electrolysis
<b>Plasma heating [32]</b>	1	4-5	Substitution from fossil fuels with a (potentially) low CO <sub>2</sub> energy source.	No direct emissions.	Depends on the local electricity mix, would be higher than indirect resistive heating due to lower efficiency.
<b>Direct resistive heating [33,34]</b>	1	3-7	Substitution fossil fuels with a (potentially) low CO <sub>2</sub> energy source.	No direct emissions.	Depends on the local electricity mix. Efficiencies as high as 90-95% have been reported which would make it one of the most efficient electrical heating options.
<b>Online Furnace Model coupled to microstructural model [20]</b>	2	4-5	CO <sub>2</sub> reduction by fuel saving.	Decrease CO <sub>2</sub> emissions up to 7% (offline tests).	No impact.

Identified technology	Related topic	TRL today	Area of action for CO <sub>2</sub> reduction	CO <sub>2</sub> emission reduction (scope 1)	CO <sub>2</sub> emission reduction (scope 2)
<b>Organic Rankine cycle [35,36]</b>	5	4-5	Substitution from the fuel that would otherwise be used to produce electricity.	No direct emissions.	Depending on the local electricity mix, e.g. 29 or 417 g <sub>CO2/kWh</sub> when comparing Sweden and Germany.
<b>Thermo-electric generator [37]</b>	5	4-5	Substitution from the fuel that would otherwise be used to produce electricity.	No direct emissions.	Depends on the local electricity mix, i.e. 29 or 417 g <sub>CO2/kWh</sub> when comparing Sweden and Germany.
<b>CCS/CCU [38,39]</b>	5	7	Capturing CO <sub>2</sub> from flue gas.	From 70% to 95%.	No impact.

## 4.1 Topic 1: Heating and burner technology

### 4.1.1 Multi-fuel burner for reheating furnaces [24,25]

This technology consists of a hybrid burner design for reheating furnaces that allows the use of different fuels, such as natural gas, hydrogen or ammonia. This technology gives the operator flexibility in fuel choice, depending on availability and price.

The CO<sub>2</sub> emissions of the system can be reduced using hydrogen or ammonia supplied from renewable sources. The CO<sub>2</sub> emissions can be reduced by up to 100% when only using ammonia or hydrogen as fuel. However, the burner can also be operated using natural gas or mixtures of natural gas, hydrogen and ammonia depending on the availability of the gases. Operating costs can also be reduced by using the cheapest energy source. Multi-fuel burners have been successfully investigated in the laboratory, but haven't been demonstrated in the long-term in industrial furnaces. Therefore, long-term operational studies are still required for this technology.

The multi-fuel burner poses some issues concerning the regulation and control of the burner, due to the difference in gas properties of the different fuels.

### 4.1.2 Biofuels as a fuel for reheating furnaces [26]

The use of biofuels such as biogas, renewable dimethyl ether (rDME) or syngas as fuel for reheating furnaces provide an opportunity for low carbon heating. The CO<sub>2</sub> footprint of biogas and rDME is higher than that of natural gas, 90.6 g<sub>CO2</sub>/MJ [1] and 66.74 g<sub>CO2</sub>/MJ [40] respectively. This would result in an increase in CO<sub>2</sub> emission of approximately 20% for rDME [27] and approximately 62% for Biogas [1,27] compared to natural gas. This technology doesn't reduce the local CO<sub>2</sub> emissions at the furnace. However, in the overall balance of the system, the net CO<sub>2</sub> emission can be zero if the carbon in the biofuel is biogenic.

Biofuels are derived from biomass coming from industrial, agricultural or household waste. Biogas is a mixture of methane and carbon dioxide produced by the organic decomposition of biomass. Syngas is mostly a mixture of carbon monoxide, hydrogen and smaller amounts of hydrocarbons, such as methane, produced by the partial combustion of biomass.

At the Björneborg Steel's free-form forge, the substitution of 20 % propane with rDME has been tested. At Calderys' Höganäs plant in Sweden, biogas has replaced the natural gas. No figures are available on the actual reduction of CO<sub>2</sub> emissions from these installations.

#### **4.1.3 Hydrogen as a fuel for reheating processes [27–29]**

Hydrogen is a promising option that offers the potential to reduce CO<sub>2</sub> emissions when substituting conventional fossil fuels or steel mill gases. In order to use hydrogen as fuel, new burners, adapted for hydrogen combustion, need to be developed.

The technology faces many challenges: The influence of hydrogen on the heating process, product heating, scaling, product quality and on the refractory of the furnace, which are currently under investigation. In addition, the hydrogen supply, transport and storage in Europe is not yet established up and fuel prices are unknown. Finally, standards and regulations for hydrogen combustion and pollutant emissions are missing.

The substitution of fossil fuels with hydrogen offers several advantages:

- Complete avoidance of CO<sub>2</sub> emissions:  
By substituting fossil fuels or process gases with green hydrogen, a significant reduction in CO<sub>2</sub> emissions can be achieved. Unlike fossil fuels, hydrogen combustion only produces water vapor as a by-product, making it a clean and environmentally friendly alternative when produced using renewable energy.
- Oxy-fuel combustion is possible, especially when on-site electrolyzers are used and oxygen is therefore available as a by-product.

However, this technology also has downsides:

- CO<sub>2</sub>-Emissions are only avoided if hydrogen is produced by regenerative energy sources.
- Hydrogen and electrolyzers are currently not available in required amounts.
- Hydrogen is difficult to store.
- The costs for hydrogen are unknown for the future.

#### **4.1.4 Ammonia as a fuel for reheating processes [30,31]**

Replacing fossil fuels with Ammonia (NH<sub>3</sub>) produced using electricity offers the advantage of low CO<sub>2</sub> emissions when replacing conventional fossil fuels. Cost considerations may arise depending on biomass or electricity prices, and NH<sub>3</sub> combustion requires additional burner adjustments compared to H<sub>2</sub> and CH<sub>4</sub> combustion. Addressing the challenge of potential NO<sub>x</sub> emissions is also crucial for sustainable NH<sub>3</sub> implementation in steel reheating processes. Direct CO<sub>2</sub> emissions can be reduced to zero by using NH<sub>3</sub> produced from renewable energy sources.

#### **4.1.5 Plasma heating [32]**

Electric plasma heaters are being considered for steel reheating due to their ability to achieve high temperatures, high power density, and control over the furnace

atmosphere. However, this technology has lower efficiency and higher maintenance costs compared to conventional electric heating solutions. The challenges include the durability of the plasma torches, scaling up the technology, and the potential for high NO<sub>x</sub> emissions.

#### **4.1.6 Direct resistive heating [33,34]**

Direct resistive heating methods, whether using DC or AC, offer advantages such as high efficiency, high power density, and fast heating rates in steel reheating processes. However, it is mainly suitable for long products with large dimensions. Overcoming the challenges of ensuring proper contact with the feedstock, particularly at higher temperatures ( $T > 1,000\text{ °C}$ ), will be critical for the successful implementation of direct resistive heating in steel reheating applications. The reduction in CO<sub>2</sub> emissions depends on the local electricity mix. Efficiencies of 90-95% have been reported, which would make it one of the most efficient electrical heating options.

### **4.2 Topic 2: Modelling of entire furnaces, Level-2 control**

#### **4.2.1 Online Furnace Model coupled to microstructural model [20]**

An online furnace model can be used to simulate the thermal behaviour and microstructure of the product in order to develop optimised operating practices, thereby reducing the fuel consumption of the furnace. This system is easy to implement in existing furnaces but requires extensive data collection. Offline tests have shown reductions in CO<sub>2</sub> emissions of up to 7%.

### **4.3 Topic 3: Sensors and controls (Level-1), standards, regulations**

No relevant low TRL measurement technologies regarding CO<sub>2</sub> emission reduction have been identified for reheating furnaces.

### **4.4 Topic 4: Materials in the furnace and product quality**

No relevant low TRL material technologies regarding CO<sub>2</sub> emission reduction have been identified for reheating furnaces.

### **4.5 Topic 5: Heat transfer, heat recovery, productivity, economy**

#### **4.5.1 Organic Rankine cycle [35,36]**

The Organic Rankine Cycle (ORC), uses sensible heat recovery from the off-gas to generate electricity. The main challenges at present are cost and safety. The CO<sub>2</sub> emission reduction potential depends on the local electricity mix (e.g. 29 g<sub>CO2</sub>/kWh for Sweden or 417 g<sub>CO2</sub>/kWh for Germany [41]).

The advantages of ORC are as follow:

- Simplicity compared to Steam Rankine Cycle: ORC is generally less complicated than the Steam Rankine Cycle. It operates at lower temperatures and pressures, allowing for the use of simpler equipment.
- Discontinuous operation is possible.

However, ORC also has a lower efficiency than the Steam Rankine Cycle. The lower efficiency is mainly due to the lower operating temperatures of the ORC.

#### **4.5.2 Thermoelectric generator [37]**

This technology consists of heat recovery from the off-gas to produce electricity. The thermoelectric generator is less complicated than the Steam Rankine Cycle or Organic

Rankine Cycle. It has low space requirement and is well suited to small and/or discontinuous heat sources. However, this technology has a very low efficiency. Cost is currently the main issue. As for the Organic Rankine Cycle the CO<sub>2</sub> emission reduction potential depends on the local electricity mix (e.g. 29 g<sub>CO2</sub>/kWh for Sweden or 417 g<sub>CO2</sub>/kWh for Germany [41]).

#### **4.5.3 CCS/CCU [38,39]**

The principle of Carbon Capture Storage (CCS) or Carbon Capture Usage (CCU) is to capture the CO<sub>2</sub> contained in the off-gases from i.e. reheating furnaces, which represents approximately 20 to 30% of the off-gas content of blast furnace gas combustion with oxy-fuel, for further storage or utilisation. Approximately 70 to 95% of this CO<sub>2</sub> can be captured in the reactor.

For example, the CO<sub>2</sub> capture technologies CASOH (for blast furnace gas) and DISPLACE (for reheating furnaces) developed and demonstrated in the C4U project have a general potential to capture up to 94% of the CO<sub>2</sub> emissions from a steel mill. Both technologies use high-temperature gas-solid separation processes, which in turn reduce the exergy penalty associated with CO<sub>2</sub> capture technology. These technologies have the ability to recover heat at very high temperatures, such as those associated with reheating furnaces. It also produces H<sub>2</sub>/N<sub>2</sub> fuel gases that can decarbonise the energy consumption of the steel mill. The project has advanced and demonstrated the TRL level to TRL 7, with the possibility of scaling up to TRL 9 through modelling [39].

## 5 References

- [1] Patrick Gniffke, Carbon Dioxide Emissions for the German Atmospheric Emission Reporting, 2022.
- [2] A. Werner, W. Sparlinek, Potenziale zur Steigerung der Energieeffizienz in einem integrierten Hüttenwerk (2007).
- [3] E. Malfa, Sustainable heating technologies for today's and tomorrow's metal industry, Duesseldorf, 2023.
- [4] E. Aries, J. Gómez Benavides, S. Mavromatis, G. Klein, G. Chronopoulos, S. Roudier, Best available techniques (BAT) reference document for the ferrous metals processing industry Industrial Emissions Directive 2010/75/EU (integrated pollution prevention and control).
- [5] European Commission, Directorate-General for Research, Innovation, B. Lindblad, Performance of reheating furnaces equipped with highly preheated air combustion technology (HPAC), Publications Office, 2005.
- [6] European Commission, Directorate-General for Research, Innovation, U. Zanusso, K. Eberwein, W. Adler, Improvement of top gas fired reheating and direct reduction furnaces for high temperature using innovative regenerative burner, Publications Office, 2009.
- [7] European Commission, Directorate-General for Research, Innovation, W. Adler, M. Dapper, E. Malfa, J. Arribas Ramirez, T. Ekman, F. Magni, V. Battaglia, E. Filippini, U. Zanusso, CO<sub>2</sub> reduction in reheating furnaces (CO<sub>2</sub>RED), Publications Office, 2011.
- [8] Tenova, TRGS Self-Regenerative Burners, <https://tenova.com/technologies/trgs-self-regenerative-burners>, accessed November 2023.
- [9] J. von Scheele, V. Žilka, Successful use of flameless oxyfuel in steel reheating.
- [10] Yusra Khalid, May Wu, Armin Silaen, Francisco Martinez, Tyamo Okosun, Bethany Worl, John Low, Chenn Zhou, Kurt Johnson, David White, Oxygen enrichment combustion to reduce fossil energy consumption and emissions in hot rolling steel production, Journal of Cleaner Production 320 (2021) 128714.
- [11] Linde AG, REBOX® HLL – High Level Lancing oxygen technology: Success story.
- [12] C.W. Lee, I.S. Kim, J.G. Hong, Combustion Using Oxygen-Lancing in a Reheating Furnace, ACS omega 6 (2021) 16905–16912.
- [13] J. von Scheele, Use of hydrogen and other pathways for decarbonization of steel production, Frankfurt, 2023.

- [14] European Commission, Directorate-General for Research, Innovation, V. Battaglia, J. Niska, V. Cuervo Piñera, M. FANTUZZI, C. Wang, A. Rensgard, D. Cifrián Riesgo, M. Ageno, T. Ekman, C. Rein, A. Della Rocca, P. Nguyen, High efficiency low NOX BFG based combustion systems in steel reheating furnaces (HELNOx-BFG) – Final report, Publications Office, 2017.
- [15] N. Schmitz, L. Sankowski, F. Kaiser, C. Schwotzer, T. Echterhof, H. Pfeifer, Towards CO<sub>2</sub>-neutral process heat generation for continuous reheating furnaces in steel hot rolling mills – A case study, *Energy* 224 (2021) 120155.
- [16] Fives Celes, High flux technology CELINE inductor.
- [17] EFD Induction GmbH, Induction heating applications: the processes, the equipment, the benefits (2010).
- [18] European Commission, Directorate-General for Research, Innovation, S. Wilcox, J. Ward, G. Andrews, Smartfire – Real-time intelligent diagnostics and optimisation of reheating furnace performance, Publications Office, 2010.
- [19] European Commission, Directorate-General for Research, Innovation, J. Niska, C. Steimer, J. Broughton, A. Queck, C. Tan, V. Santisteban Mendive, Advanced measurements and dynamic modelling for improved furnace operation and control (DYNAMO) – Final report, Publications Office, 2016.
- [20] European Commission, Directorate-General for Research, Innovation, R. Klima, M. Arribas, E. Moosavi, D. Zander, V. Santisteban, B. LEDEN, F. Vode, A. Arnaiz, F. Peñalba, M. Torkar, Quality improvement by metallurgical optimised stock temperature evolution in the reheating furnace including microstructure feedback from the rolling mill (OPTHEAT), Publications Office, 2011.
- [21] European Commission, Directorate-General for Research, Innovation, Improved atmosphere control for product quality and combustion efficiency in reheating furnaces, Publications Office, 2001.
- [22] P. Ivashechkin, M. Kozariszczuk, D. de La Fuente, T. Lapp, J.J.A. Ramirez, Novel acid dew point sensor and corrosion probes for dynamic waste heat recovery from steel mill flue gases.
- [23] J. Hellander, in: J.B. Wachtman (Ed.), *Materials & Equipment/Whitewares: Ceramic Engineering and Science Proceedings*, Volume 12, Issue 1/2, John Wiley & Sons, Inc, Hoboken, NJ, USA, 1991, pp. 162–169.
- [24] M. Bissoli, E. Malfa, D. Aszesiano, A. Della Rocca, C. Wupperman, Flexible hydrogen heating technologies with low environmental impact, Versailles, 2022.
- [25] Filippo Cirilli, Irene Luzzo, Michele Bendotti, Andrea Venturi, Characterization of side burners of reheating furnace, Versailles, 2022.
- [26] Calderys, Calderys' plant Höganäs in Sweden becomes the first Calderys site 100% powered by renewable energy, 2021, <https://calderys.com/news-and-media/calderys-plant-hoganas-sweden-becomes-first-calderys-site-100-powered-renewable>, accessed 28 November 2023.

- [27] E. Malfa, D. Astesiano, A. DellaRocca, M. Melchionda, M. Paganelli, F. Praolini (Ed.), Rolling mill decarbonization: Tenova Hydrogen SmartBurner: risultati industriali in TenarisDalmine, 2022.
- [28] Ovako, Company news reporting of decarbonisation by Hydrogen heating with Linde Burner in reheating furnace at OVAKO rolling mill, <https://www.ovako.com/en/newsevents/stories/first-in-the-world-to-heat-steel-using-hydrogen/>.
- [29] A. Della Rocca, D. Astesiano, E. Malfa, Rolling mill decarbonization: Tenova SmartBurners with 100% hydrogen, *Matériaux & Techniques* 109 (2021) 309.
- [30] Ayman M. Elbaz, Shixing Wang, Thibault F. Guiberti, William L. Roberts, Review on the recent advances on ammonia combustion from the fundamentals to the applications, *Fuel Communications* 10 (2022) 100053.
- [31] Omar I. Awad, Bo Zhou, Karim Harrath, K. Kadirgama, Characteristics of NH<sub>3</sub>/H<sub>2</sub> blend as carbon-free fuels: A review, *International Journal of Hydrogen Energy* (2022), doi:10.1016/j.ijhydene.2022.09.096.
- [32] Nicklas Tarantino, Jonas Engdahl, Andreas Johnsson et al, Plasma technology in steel industry furnaces (P49525-1) ,Final Report, 2021.
- [33] J. Davies, Institution of Electrical Engineers, Conduction and Induction Heating, P. Peregrinus Limited, 1989.
- [34] Prof. Sergio Lupi, Resistance Heating Technologies, Padova (Italy), 2015.
- [35] R. Pili, L. García Martínez, C. Wieland, H. Spliethoff, Techno-economic potential of waste heat recovery from German energy-intensive industry with Organic Rankine Cycle technology, *Renewable and Sustainable Energy Reviews* 134 (2020) 110324.
- [36] Roberto Pili, Alessandro Romagnoli, Hartmut Spliethoff, Christoph Wieland, Techno-Economic Analysis of Waste Heat Recovery with ORC from Fluctuating Industrial Sources, *Energy Procedia* 129 (2017) 503–510.
- [37] European Commission, Directorate-General for Research, Innovation, F. Mintus, S. Białek, A. Queck, A. Knox, R. Spillner, H. Domels, T. Frese, J. Esarte, Power generation from hot waste gases using thermoelectrics (PowGETEG) – Final report, Publications Office, 2020.
- [38] Cobden P, Abanades, C., International workshop on CO<sub>2</sub> capture and utilization, 2021.
- [39] Haroun Mahgerefteh, Introduction to the C4U Project: Advanced Carbon Capture for Steel Industries Integrated in CCUS Clusters, 2021.
- [40] H. Teng, J.C. McCandless, J.B. Schneyer, in: SAE Technical Paper Series, SAE International 400 Commonwealth Drive, Warrendale, PA, United States, 2004.
- [41] Olivier Corradi, Electricity Maps, [www.electricitymaps.com](http://www.electricitymaps.com).

**Acknowledgement**

This project has received funding from the Research Fund for Coal and Steel under grant agreement No 101057930.

This report reflects only the authors' view. The European Commission is not responsible for any use that may be made of the information it contains.